

Chapter 4

Time-Dependent Failure Models

- 4.1 The Weibull Distribution
- 4.2 The Normal Distribution
- 4.3 The Lognormal Distribution

4.1 The Weibull Distribution

$$\lambda(t) = at^b$$

$$\lambda(t) = \frac{\beta}{\theta} \left(\frac{t}{\theta}\right)^{\beta-1} \quad \theta > 0, \beta > 0, t \geq 0 \quad (4.1)$$

$$R(t) = \exp\left[-\int_0^t \frac{\beta}{\theta} \left(\frac{t'}{\theta}\right)^{\beta-1} dt'\right] \quad (4.2)$$

$$= e^{-(t/\theta)^\beta}$$

$$\text{and } f(t) = -\frac{dR(t)}{dt} = \frac{\beta}{\theta} \left(\frac{t}{\theta}\right)^{\beta-1} e^{-(t/\theta)^\beta} \quad (4.3)$$

$$MTTF = \theta \Gamma\left(1 + \frac{1}{\beta}\right) \quad (4.4)$$

$$\text{and } \sigma^2 = \theta^2 \left\{ \theta \Gamma\left(1 + \frac{2}{\beta}\right) - \left[\theta \Gamma\left(1 + \frac{1}{\beta}\right) \right]^2 \right\} \quad (4.5)$$

where $\Gamma(x)$ is the gamma function:

$$\Gamma(x) = \int_0^\infty y^{x-1} e^{-y} dy$$

$$\text{for } x > 0, \Gamma(x) = (x-1)\Gamma(x-1)$$

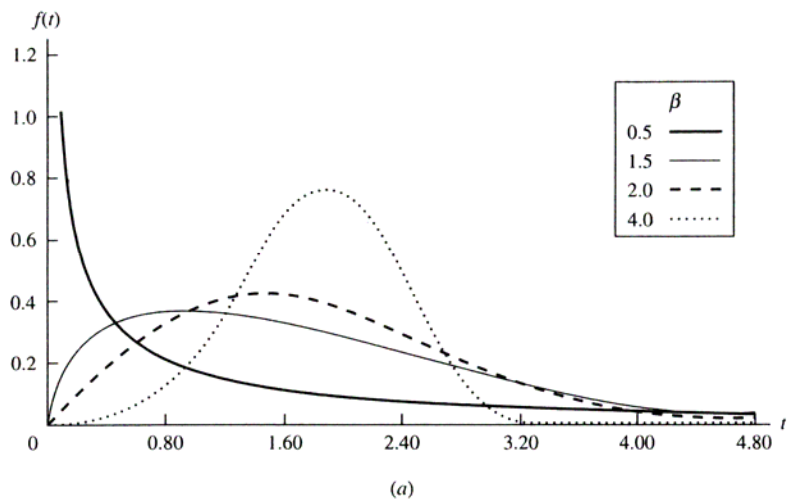


Figure 4.1a

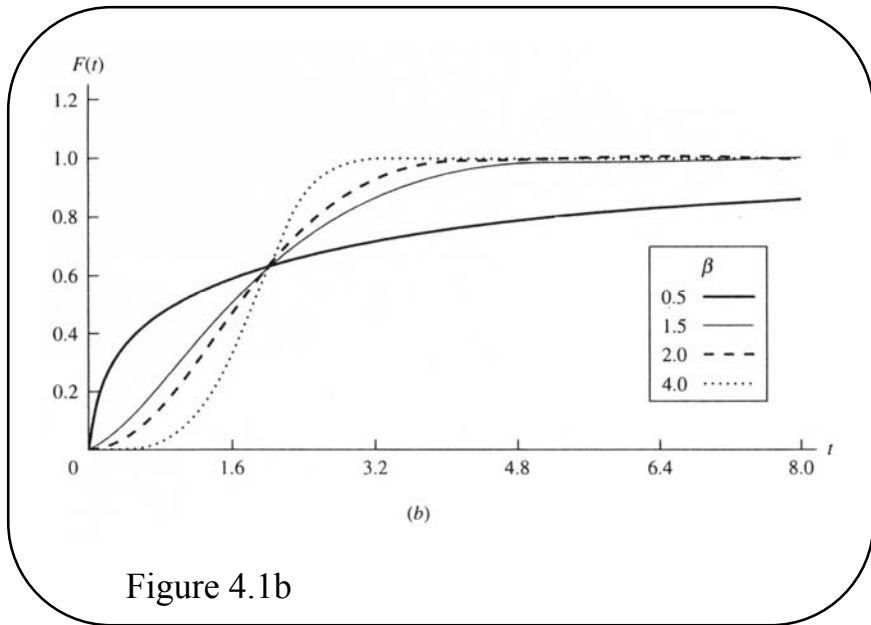


Figure 4.1b

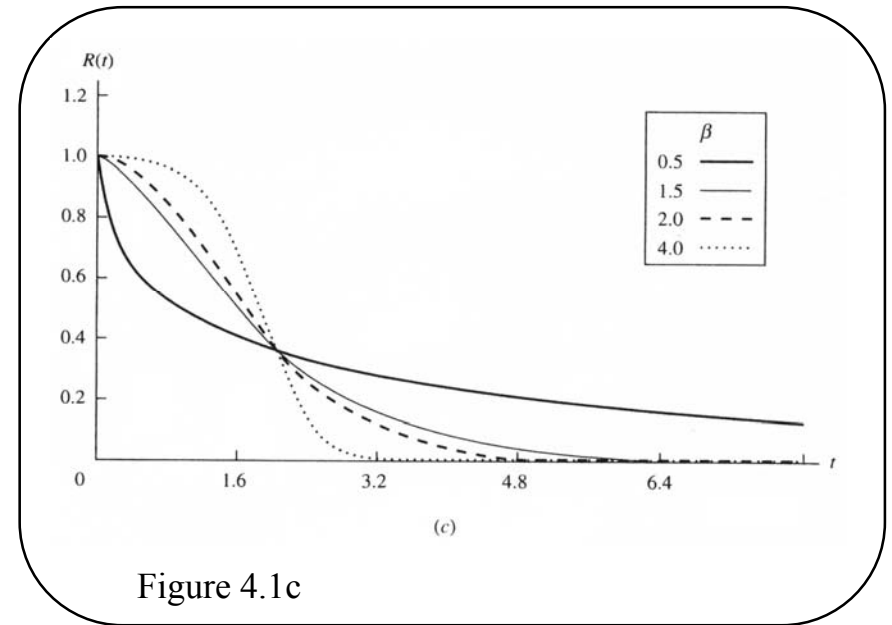


Figure 4.1c

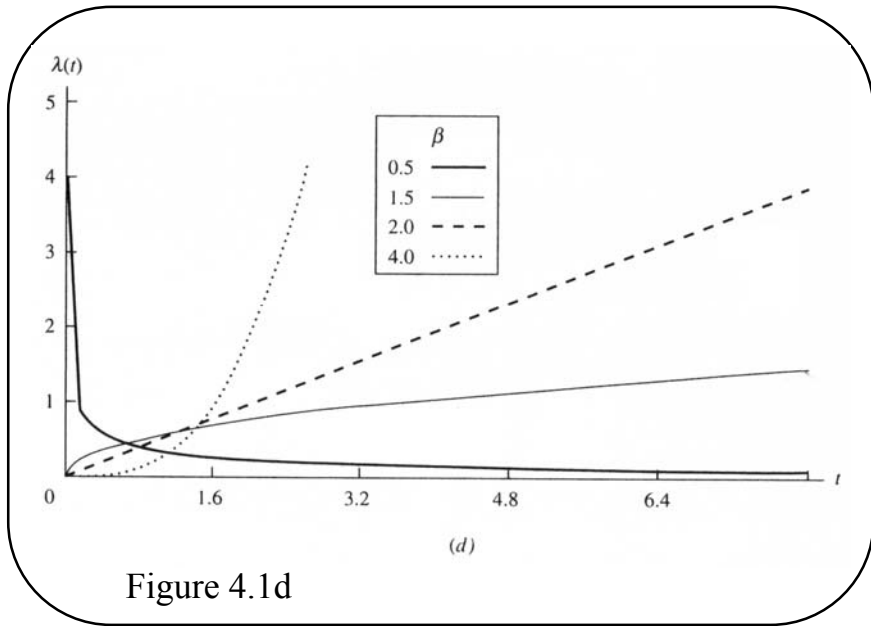


Figure 4.1d

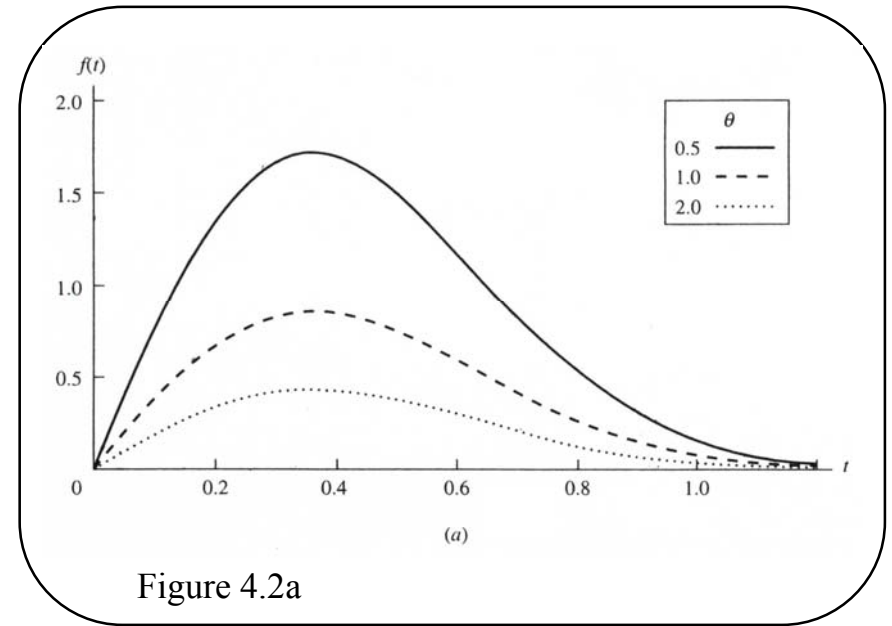


Figure 4.2a

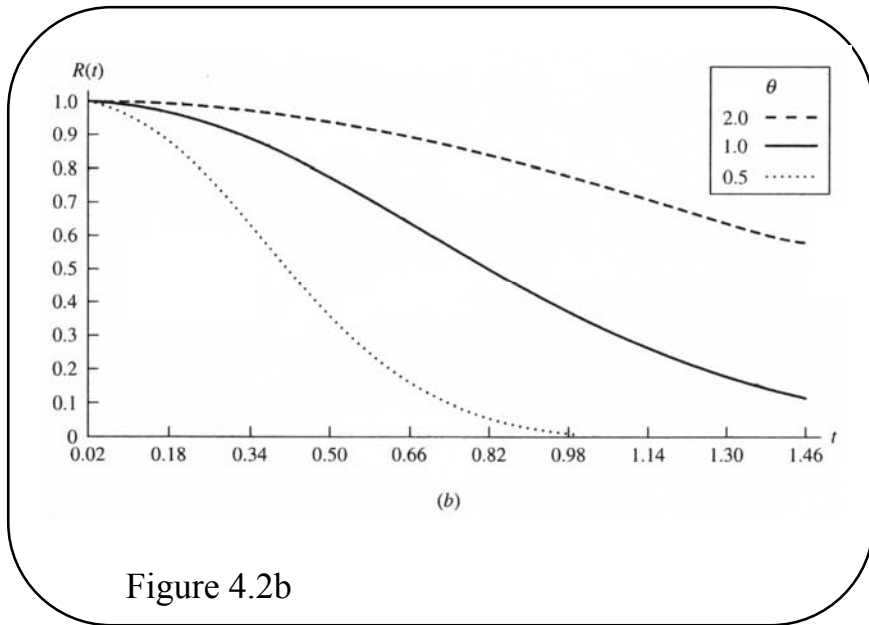


Figure 4.2b

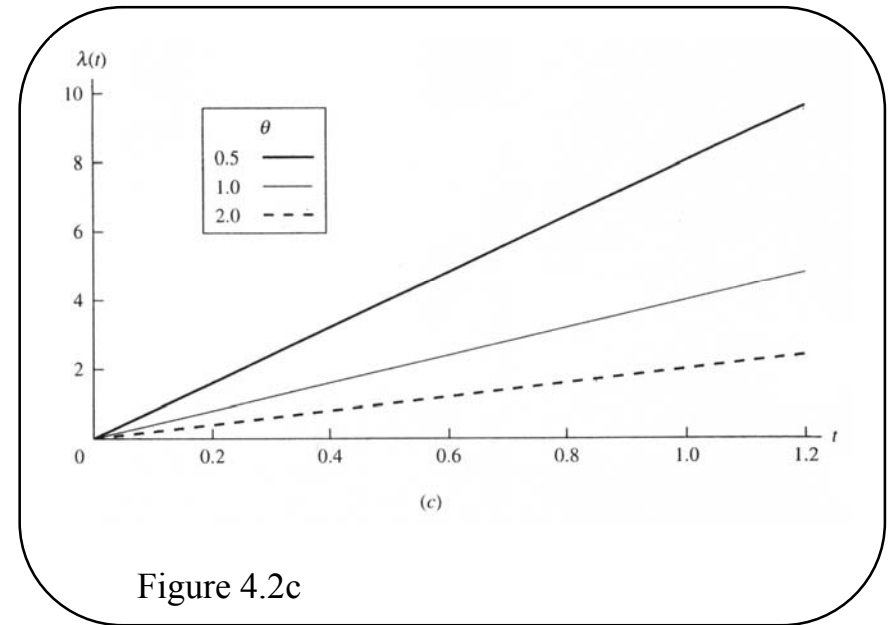


Figure 4.2c

Table 4.1 Weibull Parameter

Value	Property
$0 < \beta < 1$	Decreasing failure rate (DFR)
$\beta = 1$	Exponential distribution (CFR)
$1 < \beta < 2$	IFR, concave
$\beta = 2$	Rayleigh distribution (LFR)
$\beta > 2$	IFR, convex
$3 \leq \beta \leq 4$	IFR, Approaches normal distribution; symmetrical

Example 4.1 A compressor with a hazard rate function

$$\lambda(t) = \frac{2}{1000} \left(\frac{t}{1000} \right) = 2 \times 10^{-6} t$$

In this case, $\beta=2$, $\theta=1000$ hr.

For a desired 0.99 reliability:

$$R(t) = e^{-(t/1000)^2} = 0.99$$

The design life is given by

$$t_R = 1000 \sqrt{-\ln 99} = 100.25 \text{ hr}$$

From Eqs. (4.4) and (4.5),

$$MTTF = 1000 \Gamma \left(1 + \frac{1}{2} \right) = 886.23 \text{ hr}$$

and $\sigma^2 = 10^6 \left\{ \Gamma(1+1) - \left[\Gamma\left(1 + \frac{1}{2}\right) \right]^2 \right\}$
 $= 214,601.7$

or $\sigma = 463.25$ hr

where $\Gamma\left(1 + \frac{1}{2}\right) = 0.886227$

From Table A.9 in the Appendix.

$$\Gamma(2) = (2-1)! = 1$$

4.1.1 Design Life, Median and Mode

$$R(t) = e^{-(t/\theta)^\beta} = R$$

The design life is:

$$t_R = \theta(-\ln R)^{1/\beta} \quad (4.6)$$

The median time to failure is obtained when $R = 0.5$,

$$t_{0.50} = t_{\text{med}} = \theta(-\ln 0.5)^{1/\beta}$$

$$= \theta(0.69315)^{1/\beta} \quad (4.7)$$

Note: B1 life = $t_{0.99}$, B.1 life = $t_{0.999}$

The mode of the distribution: t^*

$$f(t^*) = \max_{t \geq 0} f(t)$$

which results in

$$t_{\text{mode}} = \begin{cases} \theta[1 - (1/\beta)]^{1/\beta} & \text{for } \beta > 1 \\ 0 & \text{for } \beta \leq 1 \end{cases} \quad (4.8)$$

Example 4.2 A failure process as a Weibull failure distribution with a shape parameter = 1/3 and a scale parameter = 16,000.

Solution:

1. The reliability function is

$$R(t) = \exp \left[- \left(\frac{t}{16,000} \right)^{1/3} \right]$$

2. $\beta = 1/3$, a decreasing failure rate indicating high infant mortality.

3. MTFF = $16,000 \Gamma\left(1 + \frac{1}{1/3}\right) = 16,000 \cdot 3! = 96,000$ hr

Since the distribution is highly skewed, the median provides a better average. The mode is zero because $\beta < 1$.

$$4. \sigma^2 = (16,000)^2 \left\{ \Gamma(7) - [\Gamma(4)]^2 \right\} = 175,104 \times 10^6$$

$$\sigma = 418.4 \times 10^3 \text{ hr}$$

5. The characteristic life is 16,000 hr. Therefore 63 percent of the failures will occur by this time.

6. If a 90 percent reliability is desired, the design life is

$$t_G = 16,000 (-\ln 0.90)^3 = 18.71 \text{ hr}$$

7. Its B1 life is $(16,000)(-\ln 0.99)^3 = 0.0162 \text{ hr}$, indicating a high percentage of early failures.

4.1.2 Burn-In Screening for Weibull

$$R(t|T_0) = \frac{\exp\left\{-\left[\frac{(t+T_0)}{\theta}\right]^\beta\right\}}{\exp\left\{-\left(\frac{T_0}{\theta}\right)^\beta\right\}} = \exp\left[-\left(\frac{t+T_0}{\theta}\right)^\beta + \left(\frac{T_0}{\theta}\right)^\beta\right]$$

For a 10-hr burn-in period:

$$R(t|10) = \exp\left[-\left(\frac{t+10}{16,000}\right)^{1/3} + \left(\frac{10}{16,000}\right)^{1/3}\right]$$

For $R = 0.90$, the design life t_R can be obtained:

$$R(t_R|10) = 0.90$$

$$t_R = 16,000 \left[-\ln 0.90 + \left(\frac{10}{16,000}\right)^{1/3} \right]^3 - 10 = 101.24 \text{ hr}$$

4.1.3 Failure Modes

For a system consisting of n components connected in series or with n independent failure modes. Each mode is an independent Weibull failure distribution with β and θ_i .

The system failure function is:

$$\lambda(t) = \sum_{i=1}^n \frac{\beta}{\theta_i} \left(\frac{t}{\theta_i}\right)^{\beta-1} = \beta t^{\beta-1} \left[\sum_{i=1}^n \left(\frac{1}{\theta_i}\right)^\beta \right] \quad (4.9)$$

with shape parameter $= \beta$, and characteristic life is:

$$\theta = \left[\sum_{i=1}^n \left(\frac{1}{\theta_i}\right)^\beta \right]^{-1/\beta}$$

Example 4.3 A system consists of five modules, where each has a Weibull failure distribution:

$$\theta = \left[\left(\frac{1}{3600}\right)^{1.5} + \left(\frac{1}{7200}\right)^{1.5} + \left(\frac{1}{5850}\right)^{1.5} + \left(\frac{1}{4780}\right)^{1.5} + \left(\frac{1}{9300}\right)^{1.5} \right]^{-1/1.5} = 1842.7$$

$$\text{and } MTTF = 1842.7 \Gamma\left(1 + \frac{2}{3}\right) = 1664.5 \text{ cycles}$$

$$t_{med} = (1842.7)(0.69315)^{1/1.5} = 1443.2 \text{ cycles}$$

The reliability function for the engine is given by

$$R(t) = \exp\left[-\left(\frac{t}{1842.7}\right)^{1.5}\right]$$

4.1.4 Identical Weibull Components

For a system consisting of n serially connected and independent components with identical failure rate functions.

$$\lambda(t) = \frac{\beta}{\theta} \left(\frac{t}{\theta} \right)^{\beta-1} \quad (4.10)$$

System failure rate is $\lambda(t) = \sum_{i=1}^n \frac{\beta}{\theta} \left(\frac{t}{\theta} \right)^{\beta-1} = \frac{n\beta}{\theta^\beta} (t)^{\beta-1}$

and $R(t) = \exp \left[-n \left(\frac{t}{\theta} \right)^\beta \right]$ (4.11)

Example 4.4 $R(150) = \exp \left[-4 \left(\frac{150}{2000} \right)^{3/4} \right] = 0.5637$

Example 4.4 A system with 4 series connectors each with a Weibull failure rate with $\beta = 3/4$ and $\theta = 2000$ hr.

System reliability at 150 hours of operation is:

$$R(150) = \exp \left[-4 \left(\frac{150}{2000} \right)^{3/4} \right] = 0.5637$$

4.1.5 The Three-Parameter Weibull

t_0 = minimum life, where $T > t_0$

This three-parameter Weibull distribution assumes that no failures exist prior to time t_0 .

$$R(t) = \exp \left[- \left(\frac{t-t_0}{\theta} \right)^\beta \right] \quad t \geq t_0 \quad (4.12)$$

and $\lambda(t) = \frac{\beta}{\theta} \left[- \left(\frac{t-t_0}{\theta} \right)^{\beta-1} \right] \quad t \geq t_0 \quad (4.13)$

t_0 = location parameter.

The variance of this distribution is the same as for the 2-parameter model, but

$$MTTF = t_0 + \theta \Gamma \left(1 + \frac{1}{\beta} \right) \quad (4.14)$$

$$t_{med} = t_0 + \theta (0.69315)^{1/\beta} \quad (4.15)$$

and the design life t_R is

$$t_R = t_0 + \theta (-\ln R)^{1/\beta} \quad (4.16)$$

To transform the 3-parameter Weibull into the 2-parameter Weibull: $t' = t - t_0$

Example 4.5: The 3-parameter Weibull has $\beta=4$, $t_0 = 100$, and $\theta = 780$.

We obtain:

$$MTTF = 100 + 780\Gamma\left(1 + \frac{1}{4}\right) = 806.99 \text{ hr}$$

$$t_{med} = 100 + 780(0.69315)^{1/4} = 811.7 \text{ hr}$$

$$\sigma^2 = (780)^2 \left\{ \Gamma\left(1 + \frac{2}{4}\right) - \left[\Gamma\left(1 + \frac{1}{4}\right) \right]^2 \right\} = 39,384.6$$

$$\sigma = 198.3 \text{ hr}$$

$$R(500) = \exp\left[-\left(\frac{500-100}{780}\right)^4\right] = 0.933$$

4.1.6 Redundancy with Weibull Failures

For a system with 2 identical and independent components connected in parallel, the system reliability is:

$$R_s(t) = 1 - [1 - R(t)]^2$$

If $R(t) = e^{-(t/\theta)^\beta}$

then $R_s(t) = 1 - [1 - e^{-(t/\theta)^\beta}]^2 = 2e^{-(t/\theta)^\beta} - e^{-2(t/\theta)^\beta} \quad (4.17)$

and $MTTF = \int_0^\infty R_s(t) dt = \int_0^\infty [2e^{-(t/\theta)^\beta} - e^{-2(t/\theta)^\beta}] dt$
 $= 2 \int_0^\infty e^{-(t/\theta)^\beta} dt - \int_0^\infty e^{-2(t/\theta)^\beta} dt$

The result is $MTTF = 2\theta\Gamma\left(1 + \frac{1}{\beta}\right) - \frac{\theta}{2^{1/\beta}}\Gamma\left(1 + \frac{1}{\beta}\right)$
 $= \theta\Gamma\left(1 + \frac{1}{\beta}\right)(2 - 2^{-1/\beta}) \quad (4.18)$

The failure rate for this system (derived in App 4D) is:

$$\lambda_s(t) = \frac{\beta}{\theta} \left(\frac{t}{\theta}\right)^{\beta-1} \frac{2 - 2e^{-(t/\theta)^\beta}}{2 - e^{-2(t/\theta)^\beta}} \quad (4.19)$$

The system does not have a Weibull failure rate. However, when t is large, the failure rate is approximated as a Weibull distribution.

Example 4.6 two fuel pumps, each has a Weibull failure distribution with $\beta = 1/2$ and $\theta = 1000$ hr.

Find system reliability for 100-hr operation and the system MTTF.

Solution:

$$R_s(t = 100) = 2 \exp\left[-\left(\frac{100}{1000}\right)^{1/2}\right] - \exp\left[-2\left(\frac{100}{1000}\right)^{1/2}\right] = 0.9265$$

$$MTTF = 1000\Gamma(3)(2 - 2^{-2}) = 3500 \text{ hr}$$

Note: A fuel pump has $R_s(t) = 0.7288$, $MTTF = 2000$

4.2 The Normal Distribution

$$f(t) = \frac{1}{\sqrt{2\pi}\sigma} \exp\left[-\frac{1}{2} \frac{(t-\mu)^2}{\sigma^2}\right] \quad -\infty < t < \infty \quad (4.20)$$

$$R(t) = \int_t^{\infty} \frac{1}{\sqrt{2\pi}\sigma} \exp\left[-\frac{1}{2} \frac{(t'-\mu)^2}{\sigma^2}\right] dt' \quad (4.21)$$

$$z = \frac{t - \mu}{\sigma}$$

$$\phi(z) = \frac{1}{\sqrt{2\pi}} e^{-z^2/2} \quad (4.22)$$

$$\Phi(z) = \int_{-\infty}^z \phi(z') dz' \quad (4.23)$$

$$F(t) = \Pr\{T \leq t\} = \Pr\left\{\frac{T - \mu}{\sigma} \leq \frac{t - \mu}{\sigma}\right\}$$

$$= \Pr\left\{z \leq \frac{t - \mu}{\sigma}\right\} = \Phi\left(\frac{t - \mu}{\sigma}\right) \quad (4.24)$$

$$R(t) = 1 - \Phi\left(\frac{t - \mu}{\sigma}\right) \quad (4.25)$$

with $F(t) = \Phi\left(\frac{t - \mu}{\sigma}\right)$

$$\lambda(t) = \frac{F(t)}{R(t)} = \frac{F(t)}{1 - \Phi((t - \mu)/\sigma)} \quad (4.26)$$

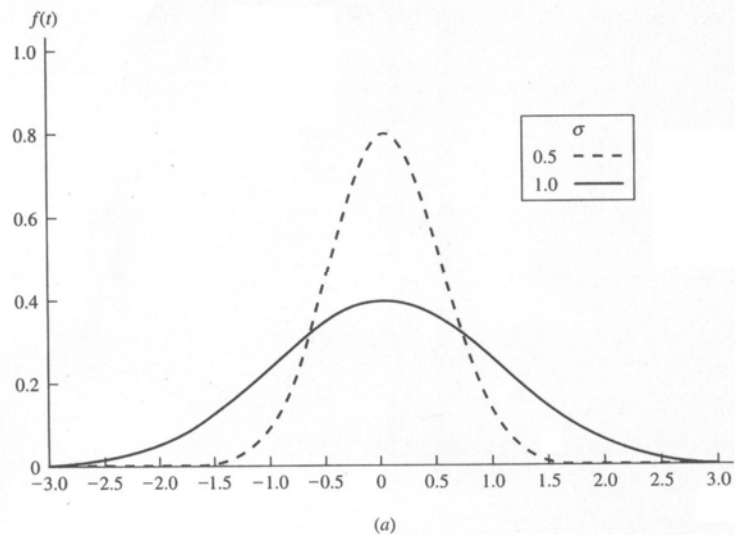


Figure 4.3a

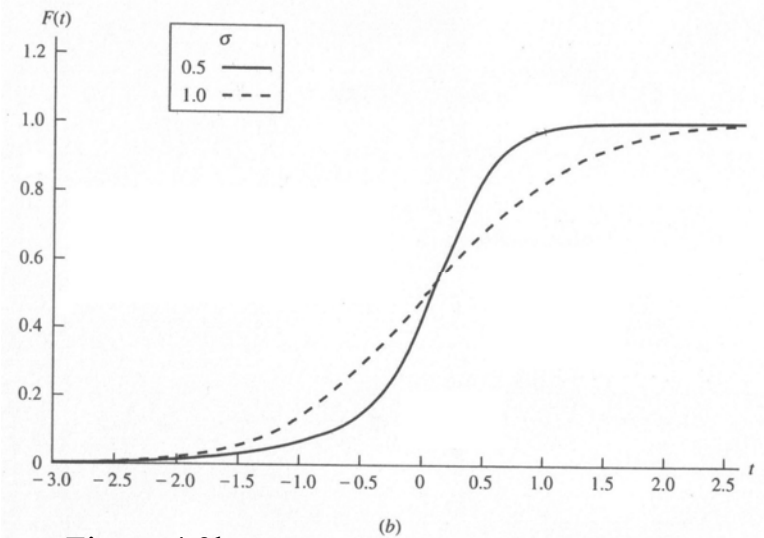


Figure 4.3b

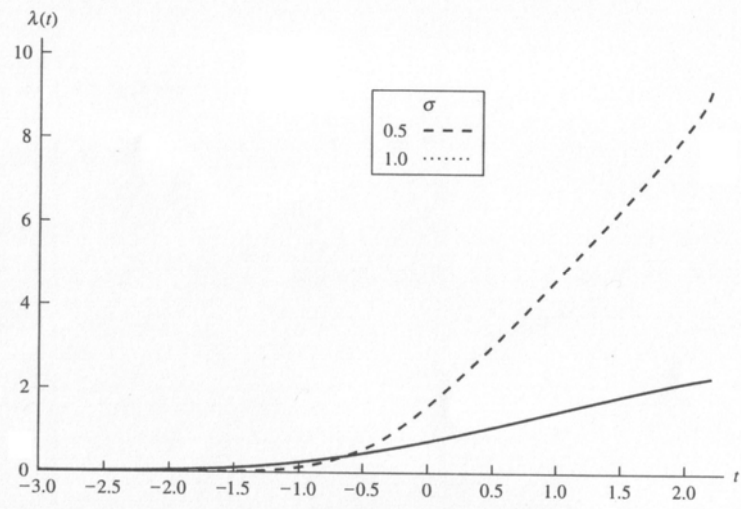


Figure 4.3c

4.3 The Lognormal Distribution

$$f(t) = \frac{1}{\sqrt{2\pi}st} \exp\left[-\frac{1}{2s^2}\left(\ln\frac{t}{t_{med}}\right)^2\right] \quad t \geq 0 \quad (4.27)$$

The mean, variance and the mode of the lognormal are:

$$MTTF = t_{med}^2 \exp[s^2/2] \quad (4.28)$$

$$\sigma^2 = t_{med}^2 \exp(s^2) [\exp(s^2) - 1] \quad (4.29)$$

$$t_{mode} = \frac{t_{med}}{\exp(s^2)} \quad (4.30)$$

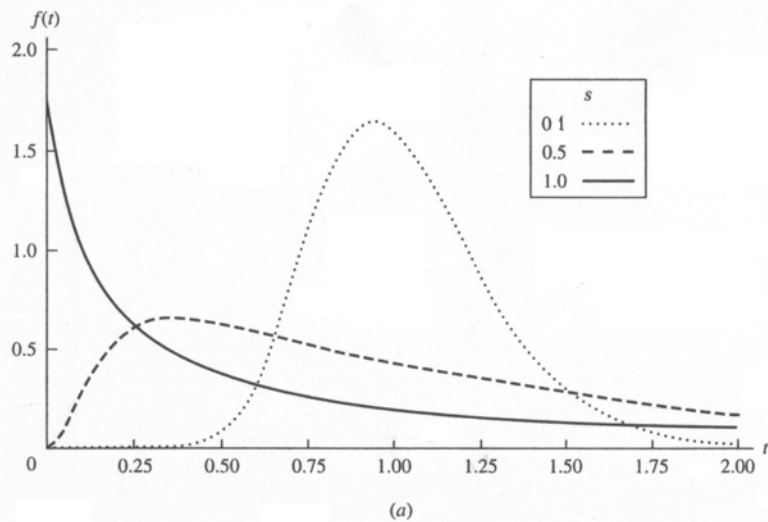


Figure 4.4a

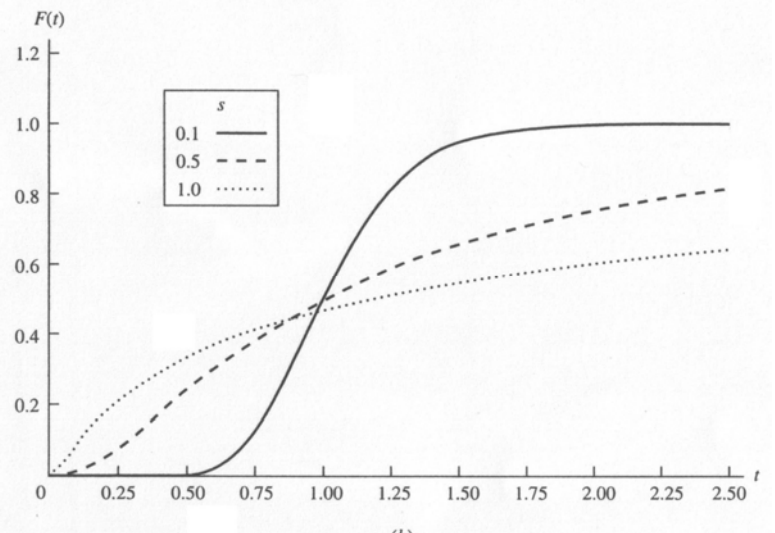


Figure 4.4b

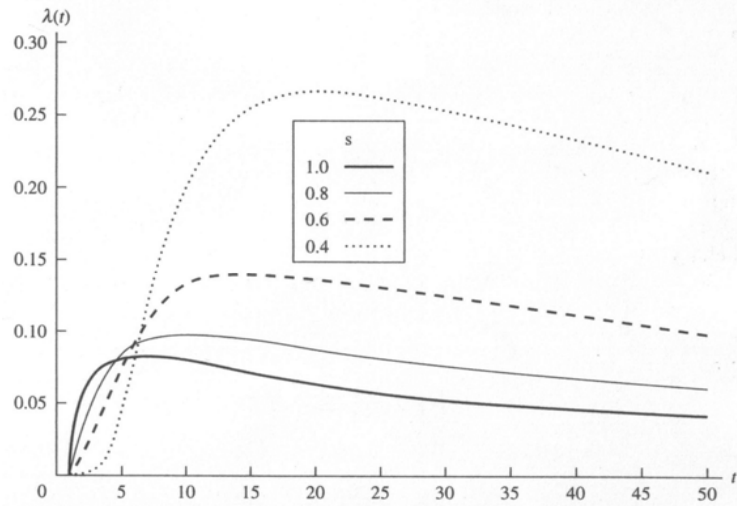


Figure 4.4c

Example 4.7

Solution:

Find $t_{0.95}$ such $\Pr \{T \geq t_{0.95}\} = 0.95$. Standardizing,

$$\Pr \left\{ z \geq \frac{t_{0.95} - 120}{14} \right\} = 1 - \Phi \left(\frac{t_{0.95} - 120}{14} \right)$$

Using the normal tables: $(t_{0.95} - 120)/14 = -1.645$, or $t_{0.95} = 96.97 \text{ hr} \approx 8 \text{ (12-hr) days}$.

Example 4.8

Solution:

We are given $\Pr \{25,000 \leq T \leq 35,000\} = 0.905$. Standardizing,

$$\Pr \left\{ \frac{25,000 - \mu}{\sigma} \leq z \leq \frac{35,000 - \mu}{\sigma} \right\} = 0.90$$

From the normal tables and the symmetry of the distribution,

$$\Pr \{-1.645 \leq z \leq 1.645\} = 0.90$$

$$\text{or } \frac{25,000 - \mu}{\sigma} = -1.645 \quad \frac{35,000 - \mu}{\sigma} = 1.645$$

$$\text{Solving, } \mu = 30,000 \quad \sigma = 3039.5$$

$$\begin{aligned} \text{Therefore } R(24,000) &= 1 - \Phi \left(\frac{24,000 - 30,000}{3039.5} \right) \\ &= 1 - \Phi(-1.97) = 0.9756 \end{aligned}$$